

# 1.85 kV Breakdown Voltage in Lateral Field-Plated $\text{Ga}_2\text{O}_3$ MOSFETs

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**Abstract**—A 400-nm thick composite field plate oxide, with a combination of atomic layer deposited and plasma enhanced chemical vapor deposited  $\text{SiO}_2$  layers, is used to enhance the breakdown voltage of spin-on-glass source/drain doped lateral  $\text{Ga}_2\text{O}_3$  MOSFET. Three terminal breakdown voltage measured in Fluorinert ambient reaches 1850 V for a  $L_{\text{gd}} = 20 \mu\text{m}$  device. This is the first report of lateral  $\text{Ga}_2\text{O}_3$  MOSFET with more than 1.8 kV breakdown voltage. For a device with  $L_{\text{gd}} = 1.8 \mu\text{m}$ , the average electric field strength is calculated to be  $2.2 \pm 0.2 \text{ MV/cm}$  while the field simulation of the device shows a peak field of 3.4 MV/cm.

**Index Terms**—Field plate, Fluorinert, spin-on-glass, gallium oxide, SOG doping, power MOSFET, air breakdown.

## I. INTRODUCTION

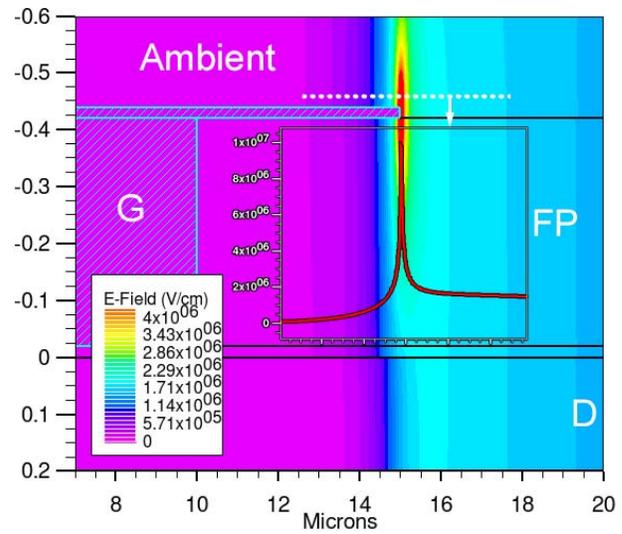
$\beta$ -GALLIUM oxide ( $\text{Ga}_2\text{O}_3$ ) has become an increasingly attractive semiconductor for next generation power electronics applications due to its high Baliga's Figure of Merit (BFoM) [1], and also due to the mature bulk crystal growth technologies [2]–[3]. Recently, high current density transistors based on delta doping [4] and nano-membrane platform [5] are demonstrated showing its low-power loss potential and for RF applications [6]. High breakdown voltage/strength MOSFETs and diodes are also reported [7]–[13]. In particular, a record average field strength of 3.8 MV/cm is measured in a lateral MOSFET [8] and the peak field strength has reached up to 5.1 MV/cm in vertical Schottky barrier diodes [9], [12]. Both data has already surpassed the theoretical limits of bulk GaN and SiC, but still far from the empirical predicted 8 MV/cm critical electric field in  $\text{Ga}_2\text{O}_3$  [1]. To date, the highest experimentally reported breakdown voltage ( $V_{BR}$ ) in lateral MOSFET is 750V with field plate [10]. In this letter, we report an improved field plate design with composite dielectrics where a high quality ALD deposited film is used in the high field region. These devices show  $V_{BR}$  beyond 1.8 kV, which demonstrates big improvements upon the previous reports,

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**Fig. 1.** Off-state TCAD electric field simulation of designed field-plated  $\text{Ga}_2\text{O}_3$  MOSFET under 1.8kV drain bias. The peak electric field at the edge of gate electrode is present both in the oxide and in the ambient, and the field strength is almost mirror symmetrical. Overlay plot shows the cross-section field strength in the ambient close to the gate electrode edge.

marking an important step towards high performance  $\text{Ga}_2\text{O}_3$  power MOSFET.

To achieve a high  $V_{BR}$  in  $\text{Ga}_2\text{O}_3$  MOSFET, it is important to not only reduce the electric field in the  $\text{Ga}_2\text{O}_3$  channel, but also make sure the peak field that is transferred to other locations does not create parasitic breakdown first. In a device, the catastrophic breakdown would not be determined by high quality  $\text{Ga}_2\text{O}_3$  channel, which might be its strongest parts; it is more likely to be determined by weaker parasitic paths such as field oxide or air. **Fig. 1** shows the off state ( $V_g = -30\text{V}$ ) electric field simulation of field-plated  $\text{Ga}_2\text{O}_3$  MOSFET under a 1.8kV drain bias using SILVACO ATLAS [14]. The dielectric constants used here are 10 for  $\text{Ga}_2\text{O}_3$  and 3.9 for  $\text{SiO}_2$  respectively [1]. And the field-plate oxide is modeled as single thick  $\text{SiO}_2$  layer. No breakdown parameters (ionization coefficients) were included in material models, thus breakdown characteristics is not simulated in the device and only electric field distribution is provided. It is seen that the peak channel field ( $\sim 1.6 \text{ MV/cm}$ ) is reduced compared to non-field plate device (not shown). The peak field is transferred into the

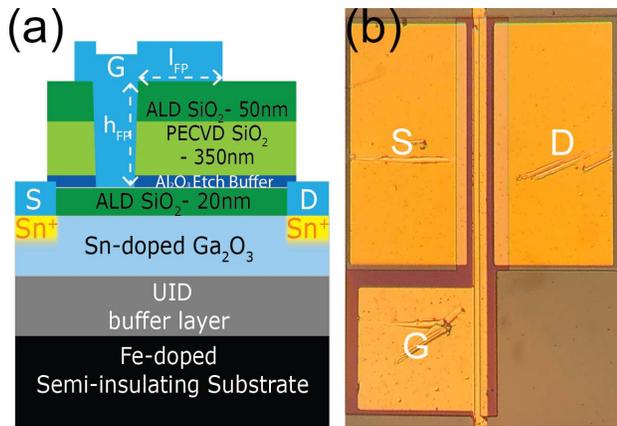


Fig. 2. (a) Cross-section view and (b) optical image of the fabricated field-plated  $\text{Ga}_2\text{O}_3$  MOSFET with SOG S/D doping.

field-plate oxide with high concentration near the field plate electrode edge. However, the critical field strength of the top layer of field plate oxide is usually unclear, and property of amorphous  $\text{SiO}_2$  varies significantly with respect to the deposition process [15]–[17]. In addition, the same peak field ( $\sim 10$  MV/cm) is also present in the ambient air, which will breakdown prematurely. Air only has a dielectric strength of 30kV/cm, 266 times lower than  $\text{Ga}_2\text{O}_3$  and 333 times lower than  $\text{SiO}_2$  [18].

In order to eliminate the extrinsic breakdown outside the channel, a composite field-plate with denser high quality ALD  $\text{SiO}_2$  at the top close to gate edge and a thick PECVD  $\text{SiO}_2$  layer in the bottom is used, as shown in Fig. 2(a). The field plate extension ( $I_{FP}$ ) was also optimized to reduce the peak field, with optimal length around halfway between gate and drain. If the breakdown happens inside field plate oxide, this design should give more  $V_{BR}$ . To prevent air breakdown, more passivation can be done, but in this letter, we used a dielectric liquid, Fluorinert (FC-770), [19]–[22] to replace air. It has approximately 4 times higher dielectric strength compared to air. Previously GaN [19]–[21] and SiC [22] devices used Fluorinert FC-77 liquid, to significantly improve  $V_{BR}$  compared to measurement in air owing to the higher dielectric breakdown strength of Fluorinert. Particularly, [19] and [20] have identified air breakdown as the pre-mature breakdown mechanism that clamped  $V_{BR}$  within 300- 400V range.

## II. FABRICATION

An MBE grown 200 nm  $2 \times 10^{17} \text{ cm}^{-3}$  Sn-doped epitaxial layer and 200 nm of UID buffer on Fe doped semi-insulating (010)  $\text{Ga}_2\text{O}_3$  substrate is used for device fabrication. The selective SOG doping of source/drain (S/D) is carried out as described in [7]. Ti/Au S/D contacts is then deposited in the doped region, followed by a 470°C ohmic annealing. A total of 420 nm of composite ALD/PECVD/ALD oxide layer is deposited on the sample (Fig. 2(a)). Both the top 50 nm field plate oxide and 20 nm gate dielectric  $\text{SiO}_2$  are deposited by plasma enhanced ALD at 300 °C under 10 mT pressure, with Tris(dimethylamino)silane (3DMAS) precursor and  $\text{O}_2$  plasma. The remaining 350 nm of  $\text{SiO}_2$  field plate oxide is

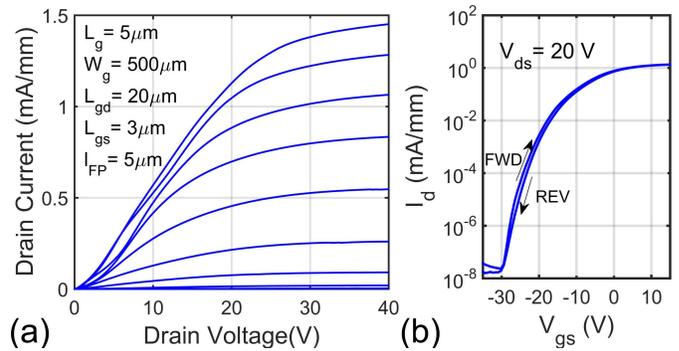


Fig. 3. (a) Output current-voltage characteristic (–20V to 12V with 4V step) and (b) transfer characteristic of fabricated field plated MOSFET with Spin-on-Glass S/D doping.

deposited by PECVD at 250 °C and 900 mT using  $\text{SiH}_4$  and  $\text{N}_2\text{O}$  gases, while thin  $\text{Al}_2\text{O}_3$  etch stop is deposited by thermal ALD at 300 °C using Tri-methyl Aluminum (TMA) and  $\text{H}_2\text{O}$ . A highly selective  $\text{CF}_4$  based reactive ion etch (RIE) is then used to form the gate trench in the field plate oxide, where extremely low pressure and high ICP power is tuned to ensure a synergic etch for smooth bottom [23], a high selectivity over  $\text{Al}_2\text{O}_3$  [24] and to form a nearly vertical sidewall profile. The  $\text{Al}_2\text{O}_3$  layer is wet etched in photo-resist developer. This etch is followed by another 450°C 1 minute RTA to densify the stack. At last, 550nm of Ti/Al/Ni/Au contact is realigned to the trench, forming the field plate structure as shown in Fig. 2(a). Devices are finally isolated by a  $\text{BCl}_3/\text{Ar}$  RIE, which created a  $\sim 220\text{nm}$  recess surrounding active region. Fig. 2(b) shows an optical image of fabricated device.

## III. RESULTS AND DISCUSSION

DC I-V characteristics are measure with HP 4155B semiconductor parameter analyzer and is shown in Fig. 3. Fig. 3(b) shows 0.8 V hysteresis in the gate voltage forward and reverse sweep. The effective channel carrier density extracted from differential CV analysis is  $\sim 1.5 \times 10^{16} / \text{cm}^3$  [25], [26]. The reduced effective carrier density compared to initial doping density is due to the out diffusion of dopant during spin-on-glass drive-in annealing [7], [27]. The unexpected large negative  $V_{th}$  is attributed to possible charge in the oxide stack introduced during RIE process and temperature variations on the sample during the SOG drive-in annealing, thus the differential CV carrier density may not correspond to the carrier density in the FET channel. Moreover, subthreshold swing analysis gives a  $D_{it} \sim 2.0 \times 10^{13} / \text{cm}^2 \cdot \text{eV}$ . The three terminal breakdown test is performed with a custom setup combining HP 4155B and Keithley 2657A high-voltage source-meter. For device shown in Fig. 3 with  $L_{gd} = 20 \mu\text{m}$ , the first breakdown measurement is performed with sample submerged in Fluorinert FC-770 to reduce air breakdown potential. The drain is swept from 0V to 2 kV with catastrophic breakdown measured at 1850 V. This is the highest breakdown voltage measured in a lateral  $\text{Ga}_2\text{O}_3$  MOSFET to date. After the first sweep, the sample is taken out of Fluorinert and exposed in the air. Another breakdown test is performed in air, and device

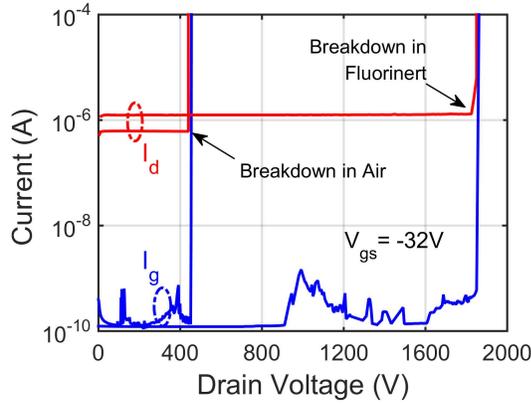


Fig. 4. Three-terminal breakdown measurement data from device under test (DUT) shown in Fig. 3. Two neighboring devices with same dimensions are measured respectively in Fluorinert and Air.

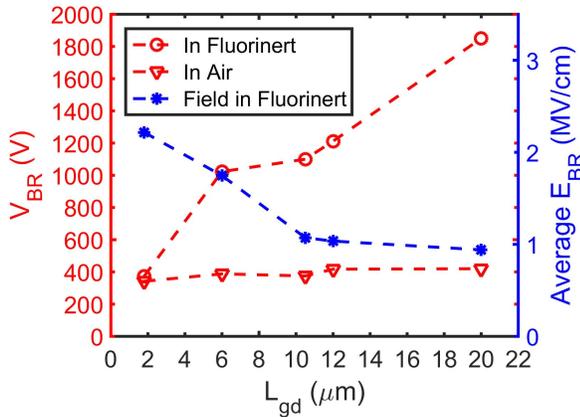


Fig. 5. Breakdown voltage  $V_{BR}$  and averaged breakdown electric field  $E_{BR}$  vs gate-drain separation  $L_{gd}$  in measured devices. The averaged breakdown field in Ga<sub>2</sub>O<sub>3</sub> channel (blue asterisks, labeled “field in Fluorinert”) is calculated by dividing the sum of  $V_{BR}$  (measured in Fluorinert) and  $V_g$  over  $L_{gd}$ . All  $L_{gd}$  data is verified by SEM images.

had catastrophic breakdown at 440V. Both breakdown test data is shown in Fig. 4. The difference of  $V_{BR}$  with and without Fluorinert clearly shows that the breakdown without Fluorinert first happened in the air and is extrinsic to the channel.

With varying gate-drain spacing  $L_{gd}$ , multiple breakdown voltage is measured with and without Fluorinert. The average breakdown strength is also calculated by dividing net gate-drain voltage ( $V_{BR}-V_g$ ) over  $L_{gd}$  [8] and is displayed in Fig. 5. As shown in Fig. 5, all devices measured a higher  $V_{BR}$  with Fluorinert, and the  $V_{BR}$  with Fluorinert is approximately 4 times higher than  $V_{BR}$  measured in the air at higher  $L_{gd}$ . Moreover, it can be seen that as  $L_{gd}$  gets smaller,  $E_{BR}$  increases rapidly. By pushing the gate and drain closer, the high field region is going to occupy more portion of the  $L_{gd}$ . For a device with  $L_{gd} = 1.8\mu\text{m}$ , the average electric field strength is calculated to be  $2.2 \pm 0.2$  MV/cm and the ATLAS simulation of the device shows a peak field of 3.4 MV/cm. Moreover, due to the speculated extrinsic breakdown, the averaged field strength of  $2.2 \pm 0.2$  MV/cm merely sets a lower bound for intrinsic Ga<sub>2</sub>O<sub>3</sub> breakdown strength. Careful device engineering bearing the extrinsic breakdown in mind can push

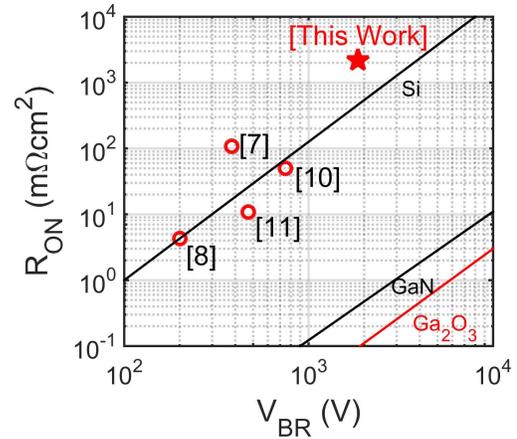


Fig. 6. Plot of  $R_{ON}$  vs.  $V_{BR}$  of DUT figure of merit against previously published lateral Ga<sub>2</sub>O<sub>3</sub> MOSFETs.  $R_{on}$  in this work is calculated at  $V_{ds} = 10$  V.

the breakdown even higher. Fig. 6 shows a comparison of  $R_{on}$  and  $V_{BR}$  in published lateral Ga<sub>2</sub>O<sub>3</sub> MOSFETs.

#### IV. CONCLUSION

A composite field-plate design and Fluorinert ambient is used to effectively reduce the extrinsic breakdown potential, especially in the air. Three-terminal breakdown voltage of 1850 V is measured in a composite-field-plated Ga<sub>2</sub>O<sub>3</sub> MOSFET with  $L_{gd} = 20\mu\text{m}$ . The breakdown voltage shows a big improvement upon previous reports, indicating the immense potential of Ga<sub>2</sub>O<sub>3</sub> for high-voltage power electronics applications.

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#### REFERENCES

- [1] M. Higashiwaki, K. Sasaki, H. Murakami, Y. Kumagai, A. Koukitsu, A. Kuramata, T. Masui, and S. Yamakoshi, “Recent progress in Ga<sub>2</sub>O<sub>3</sub> power devices,” *Semicond. Sci. Technol.*, vol. 31, no. 3, p. 34001, 2016, doi: 10.1088/0268-1242/31/3/034001.
- [2] H. Aida, K. Nishiguchi, H. Takeda, N. Aota, K. Sunakawa, and Y. Yaguchi, “Growth of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> single crystals by the edge-defined, film fed growth method,” *Jpn. J. Appl. Phys.*, vol. 47, no. 11R, pp. 8506–8509, Nov. 2008, doi: 10.1143/JJAP.47.8506.
- [3] K. Irmischer, Z. Galazka, M. Pietsch, R. Uecker, and R. Fornari, “Electrical properties of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> single crystals grown by the Czochralski method,” *J. Appl. Phys.*, vol. 110, no. 6, p. 063720, 2011, doi: 10.1063/1.3642962.
- [4] Z. Xia, C. Joishi, S. Krishnamoorthy, S. Bajaj, Y. Zhang, M. Brenner, S. Lodha, and S. Rajan, “Delta doped  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> field effect transistors with regrown ohmic contacts,” *IEEE Electron Device Lett.*, vol. 39, no. 4, pp. 568–571, Apr. 2018, doi: 10.1109/LED.2018.2805785.
- [5] H. Zhou, K. Maize, G. Qiu, A. Shakouri, and P. D. Ye, “ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> on insulator field-effect transistors with drain currents exceeding 1.5 A/mm and their self-heating effect,” *Appl. Phys. Lett.*, vol. 111, no. 9, p. 092102, 2017, doi: 10.1063/1.5000735.
- [6] A. J. Green, K. D. Chabak, M. Baldini, N. Moser, R. Gilbert, R. C. Fitch, G. Wagner, Z. Galazka, J. Mccandless, A. Crespo, K. Leedy, and G. H. Jessen, “ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> MOSFETs for radio frequency operation,” *IEEE Electron Device Lett.*, vol. 38, no. 6, pp. 790–793, Jun. 2017, doi: 10.1109/LED.2017.2694805.

- [7] K. Zeng, J. S. Wallace, C. Heimbürger, K. Sasaki, A. Kuramata, T. Masui, J. A. Gardella, and U. Singiseti, "Ga<sub>2</sub>O<sub>3</sub> MOSFETs using spin-on-glass source/drain doping technology," *IEEE Electron Device Lett.*, vol. 38, no. 4, pp. 513–516, Apr. 2017, doi: [10.1109/LED.2017.2675544](https://doi.org/10.1109/LED.2017.2675544).
- [8] A. J. Green, K. D. Chabak, E. R. Heller, R. C. Fitch, M. Baldini, A. Fiedler, K. Irmscher, G. Wagner, Z. Galazka, S. E. Tetlak, A. Crespo, K. Leedy, and G. H. Jessen, "3.8-MV/cm breakdown strength of MOVPE-grown Sn-doped  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> MOSFETs," *IEEE Electron Device Lett.*, vol. 37, no. 7, pp. 902–905, Jul. 2016, doi: [10.1109/LED.2016.2568139](https://doi.org/10.1109/LED.2016.2568139).
- [9] K. Konishi, K. Goto, H. Murakami, Y. Kumagai, A. Kuramata, S. Yamakoshi, and M. Higashiwaki, "1-kV vertical Ga<sub>2</sub>O<sub>3</sub> field-plated Schottky barrier diodes," *Appl. Phys. Lett.*, vol. 110, no. 10, p. 103506, 2017, doi: [10.1063/1.4977857](https://doi.org/10.1063/1.4977857).
- [10] M. H. Wong, K. Sasaki, A. Kuramata, S. Yamakoshi, and M. Higashiwaki, "Field-plated Ga<sub>2</sub>O<sub>3</sub> MOSFETs with a breakdown voltage of over 750 V," *IEEE Electron Device Lett.*, vol. 37, no. 2, pp. 212–215, Feb. 2016, doi: [10.1109/LED.2015.2512279](https://doi.org/10.1109/LED.2015.2512279).
- [11] K. D. Chabak, J. P. McCandless, N. A. Moser, A. J. Green, K. Mahalingam, A. Crespo, N. Hendricks, B. M. Howe, S. E. Tetlak, K. Leedy, R. C. Fitch, D. Wakimoto, K. Sasaki, A. Kuramata, and G. H. Jessen, "Recessed-gate enhancement-mode  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> MOSFETs," *IEEE Electron Device Lett.*, vol. 39, no. 1, pp. 67–70, Jan. 2018, doi: [10.1109/LED.2017.2779867](https://doi.org/10.1109/LED.2017.2779867).
- [12] X. Yan, I. S. Esqueda, J. Ma, J. Tice, H. Wang, X. Yan, I. S. Esqueda, J. Ma, J. Tice, and H. Wang, "High breakdown electric field in  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/graphene vertical barristor heterostructure," *Appl. Phys. Lett.*, vol. 112, no. 3, p. 032101, 2018, doi: [10.1063/1.5002138](https://doi.org/10.1063/1.5002138).
- [13] J. Yang, S. Ahn, F. Ren, S. J. Pearton, S. Jang, J. Kim, and A. Kuramata, "High reverse breakdown voltage Schottky rectifiers without edge termination on Ga<sub>2</sub>O<sub>3</sub>," *Appl. Phys. Lett.*, vol. 110, no. 19, p. 192101, 2017, doi: [10.1063/1.4983203](https://doi.org/10.1063/1.4983203).
- [14] *Atlas User's Manual*. Silvaco Int., Santa Clara, CA, USA, 2014.
- [15] F. Hirose, Y. Kinoshita, S. Shibuya, Y. Narita, Y. Takahashi, H. Miya, K. Hirahara, Y. Kimura, and M. Niwano, "Atomic layer deposition of SiO<sub>2</sub> from Tris(dimethylamino)silane and ozone by using temperature-controlled water vapor treatment," *Thin Solid Films*, vol. 519, no. 1, pp. 270–275, 2010, doi: [10.1016/j.tsf.2010.07.107](https://doi.org/10.1016/j.tsf.2010.07.107).
- [16] T. Usui, C. A. Donnelly, M. Logar, R. Sinclair, J. Schoonman, and F. B. Prinz, "Approaching the limits of dielectric breakdown for SiO<sub>2</sub> films deposited by plasma-enhanced atomic layer deposition," *Acta Mater.*, vol. 61, no. 20, pp. 7660–7670, 2013, doi: [10.1016/j.actamat.2013.09.003](https://doi.org/10.1016/j.actamat.2013.09.003).
- [17] S.-J. Won, S. Suh, M. S. Huh, and H. J. Kim, "High-quality low-temperature silicon oxide by plasma-enhanced atomic layer deposition using a metal-organic silicon precursor and oxygen radical," *IEEE Electron Device Lett.*, vol. 31, no. 8, pp. 857–859, Aug. 2010, doi: [10.1109/LED.2010.2049978](https://doi.org/10.1109/LED.2010.2049978).
- [18] *Dielectric Strength of Air*. Accessed: Jul. 27, 2018. [Online]. Available: <https://hypertextbook.com/facts/2000/AliceHong.shtml>
- [19] N. Tipirneni, A. Koudymov, V. Adivarahan, J. Yang, G. Simin, and M. A. Khan, "The 1.6-kV AlGaIn/GaN HFETs," *IEEE Electron Device Lett.*, vol. 27, no. 9, pp. 716–718, Sep. 2006, doi: [10.1109/LED.2006.881084](https://doi.org/10.1109/LED.2006.881084).
- [20] Y. Dora, A. Chakraborty, L. McCarthy, S. Keller, S. P. DenBaars, and U. K. Mishra, "High breakdown voltage achieved on AlGaIn/GaN HEMTs with integrated slant field plates," *IEEE Electron Device Lett.*, vol. 27, no. 9, pp. 713–715, Sep. 2006, doi: [10.1109/LED.2006.881020](https://doi.org/10.1109/LED.2006.881020).
- [21] K. Nomoto, B. Song, Z. Hu, M. Zhu, M. Qi, N. Kaneda, T. Mishima, T. Nakamura, D. Jena, and H. G. Xing, "1.7-kV and 0.55-m $\Omega$ -cm<sup>2</sup> GaN p-n diodes on bulk GaN substrates with avalanche capability," *IEEE Electron Device Lett.*, vol. 37, no. 2, pp. 161–164, Feb. 2016, doi: [10.1109/LED.2015.2506638](https://doi.org/10.1109/LED.2015.2506638).
- [22] A. K. Agarwal, J. B. Casady, L. B. Rowland, W. F. Valek, M. H. White, and C. D. Brandt, "1.1 kV 4H-SiC power UMOSFETs," *IEEE Electron Device Lett.*, vol. 18, no. 12, pp. 586–588, Dec. 1997, doi: [10.1109/55.644079](https://doi.org/10.1109/55.644079).
- [23] L. Zhang, A. Verma, H. Xing, and D. Jena, "Inductively-coupled-plasma reactive ion etching of single-crystal  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>," *Jpn. J. Appl. Phys.*, vol. 56, no. 3, p. 030304, 2017, doi: [10.7567/JJAP.56.030304](https://doi.org/10.7567/JJAP.56.030304).
- [24] S. Tegen and P. Moll, "Etch Characteristics of Al<sub>2</sub>O<sub>3</sub> in ICP and MERIE plasma etchers," *J. Electrochem. Soc.*, vol. 152, no. 4, pp. G271–G276, 2005, doi: [10.1149/1.1865912](https://doi.org/10.1149/1.1865912).
- [25] Y. Jia, K. Zeng, J. S. Wallace, J. A. Gardella, and U. Singiseti, "Spectroscopic and electrical calculation of band alignment between atomic layer deposited SiO<sub>2</sub> and  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> (201)," *Appl. Phys. Lett.*, vol. 106, no. 10, p. 102107, 2015, doi: [10.1063/1.4915262](https://doi.org/10.1063/1.4915262).
- [26] D. K. Schroder, *Semiconductor Material and Device Characterization*, 3rd ed. Hoboken, NJ, USA: Wiley, 2006.
- [27] M. H. Wong, K. Sasaki, A. Kuramata, S. Yamakoshi, and M. Higashiwaki, "Anomalous Fe diffusion in Si-ion-implanted  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> and its suppression in Ga<sub>2</sub>O<sub>3</sub> transistor structures through highly resistive buffer layers," *Appl. Phys. Lett.*, vol. 106, no. 3, p. 032105, 2015, doi: [10.1063/1.4906375](https://doi.org/10.1063/1.4906375).