

# Introduction to (Great Lakes) Water Quality Modeling

Ecosystem Restoration Workshop  
June 2008

# Basic idea

- ❖ Based on fundamental “truths”, usually stated in terms of conservation of a particular property
  - e.g. mass, momentum, energy
    - Mass is neither created nor destroyed, but may change form
    - Momentum is governed by certain physical laws (such as Newton’s laws), reacts to forces
    - Energy also is conserved, but may change form, such as potential ↔ kinetic

❖ Most physical models based on rate expressions –

- For example, consider the process of filling a tank with water; how would you answer the question, “What is the volume of water in the tank at any given time?”
  - The rate at which water is being added to (or leaking from) the tank should, intuitively, be part of the answer
  - In general, some initial starting point (initial condition) also needs to be known in order to calculate a history of water volume

## ❖ Formalization of problem in mathematical terms –

- We can't start with  $V$  (volume) = \_\_\_\_\_ , since we don't know enough to start with
- What do we know?
  - [Rate of change of  $V$ ] = [filling rate] – [leaking rate]

$$\frac{dV}{dt} = Q_{in} - Q_{out}$$

( $Q$  = flowrate)

$$\frac{dV}{dt} = Q_{in} - Q_{out}$$

❖ This is a simple first-order initial value problem, which can be solved if we know the flow values and initial condition

- Let the initial volume be  $V_0$
- Assume the inflow rate is constant
- Assume the outflow rate is proportional to  $V$
- Then,

$$Q_{out} = kV \qquad \frac{dV}{dt} + kV = Q_{in}$$

$$\frac{dV}{dt} + kV = Q_{in}$$

- ❖ With the above assumptions, and if  $k$  is approximately constant (in reality it is a function of  $V$ ), this equation happens to have an analytical solution
- ❖ More complicated problems that may not have an analytical solution are usually solved using numerical integration

# Concentration changes

❖ Now consider the problem of changing concentration of a particular substance in a reactor (jar, tank, stream, lake, etc.);

➤ [rate of change of mass] =

[rate of transport in]

- [rate of transport out]

+ (-) [net rate of transformation or production]

Note concept of control volume used here; also, “transport” includes both advective and diffusive processes.

# Mathematical statement

$$\frac{dM}{dt} = \frac{d(CV)}{dt} = (QC)_{in} - (QC)_{out} - w_s CA - KCV$$

(+ dispersion)

$M$  = mass

$C$  = concentration

$w_s$  = settling rate (if applicable)

$A$  = bottom area

$K$  = first-order decay (growth) rate (if applicable)

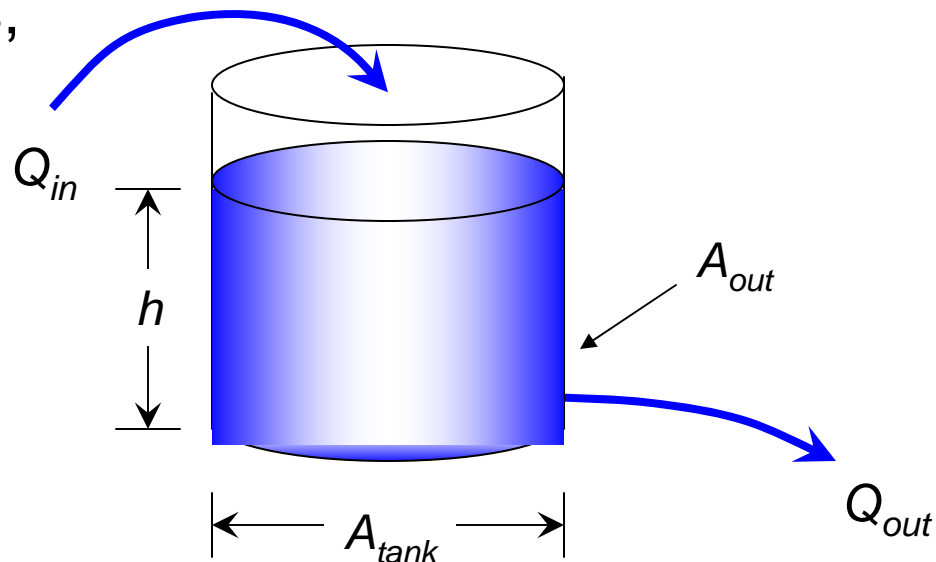
# Stella application

## ❖ Tank filling example:

Recall 
$$\frac{dV}{dt} + kV = Q_{in}$$

From basic application of energy and mass conservation principles,

$$k \cong \sqrt{\frac{2g}{h}} \frac{A_{out}}{A_{tank}}$$



- ❖ If  $h$  is assumed to change only very slowly, then  $k$  is approximately constant ( $k$  is really a function of  $V$ ) and an analytical solution may be obtained,

$$V \cong V_0 e^{-kt} + \frac{Q_{in}}{k}$$

- ❖ A steady state solution is found when  $d/dt \rightarrow 0$  or  $t \rightarrow \infty$ ,

$$V_{steady} = \frac{Q_{in}}{k}$$

# Numerical solution

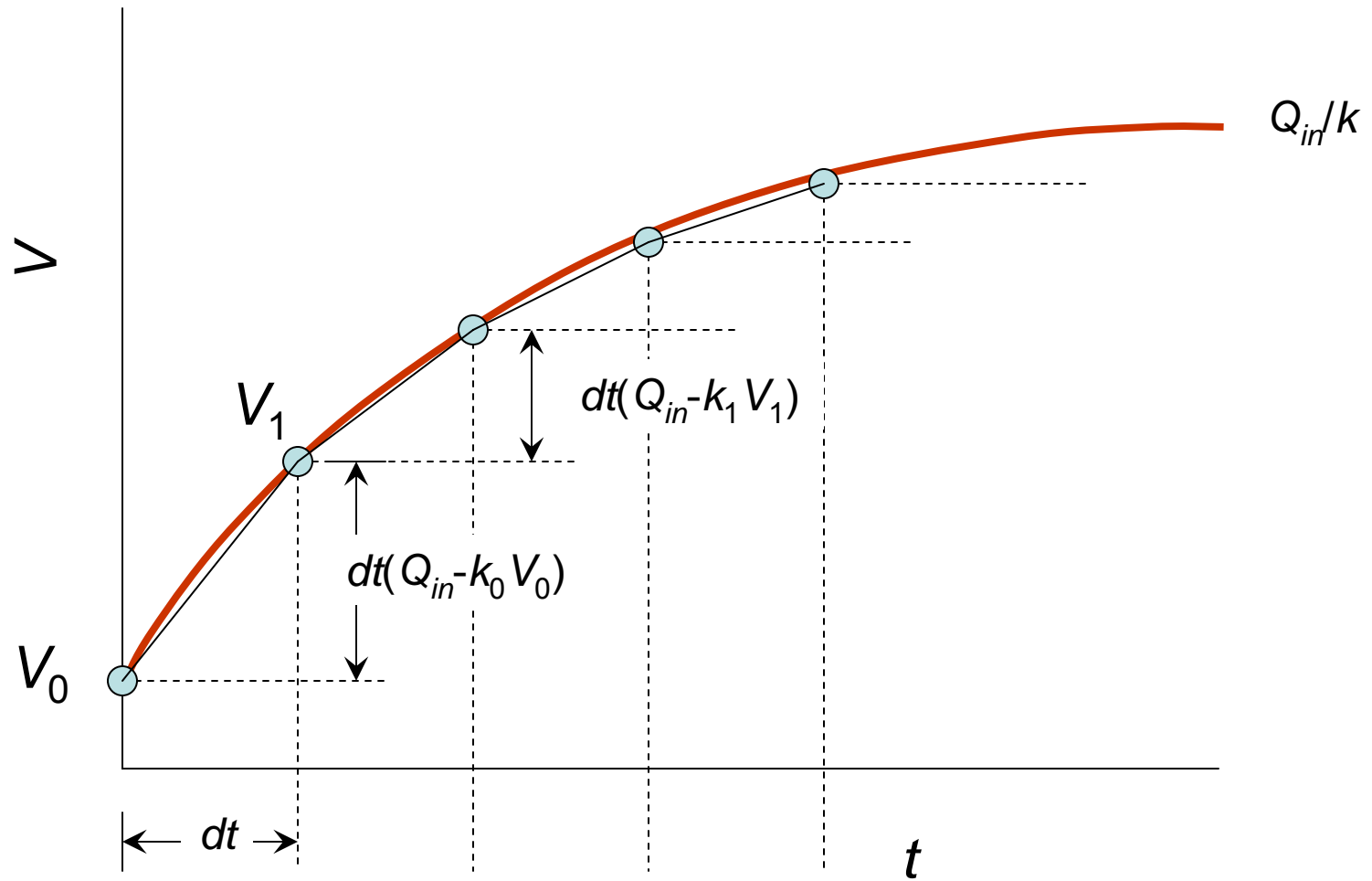
❖ (perhaps better in this case, since fewer approximations)

❖ write

$$\frac{dV}{dt} + kV = Q_{in} \quad \Rightarrow \quad dV = dt \underbrace{(Q_{in} - kV)}_{\text{rate}}$$

$$V_{i+1} = V_i + dt * (Q_{in} - k_i V_i)$$

$$V_{i+1} = V_i + dt * (Q_{in} - k_i V_i)$$



# Concentration model

❖ Now consider the issue of changing concentration, still in a mixed reactor

➤ From before, assume  $Q_{in} = Q_{out} = Q$  (so,  $V$  is constant)

$$\frac{dM}{dt} = \frac{d(CV)}{dt} = \boxed{(QC)_{in}} - (QC)_{out} - w_s CA - KCV$$

Often called loading,  $W$

$$\frac{dC}{dt} = \frac{QC_{in}}{V} - C \frac{(Q + w_s A + KV)}{V}$$

$$\Rightarrow C = C_0 e^{-\lambda t} + \frac{QC_{in}}{\lambda V}, \quad \lambda = \frac{Q + w_s A + KV}{V}$$

(for constant coefficients)

# Multiple reactors

## ❖ Add dispersion to account for exchange between reactors

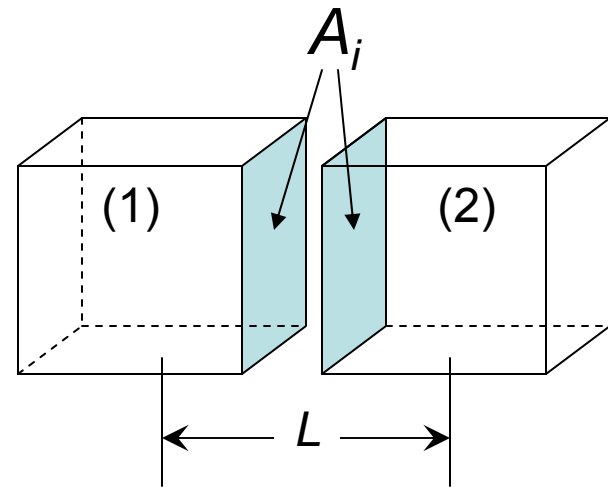
### ➤ Dispersive transport:

$L$  = distance over which change in  $C$  occurs  
(usually taken as distance between centers of reactors)

$A_i$  = interfacial area between reactors, over which dispersion occurs

$E'$  = bulk dispersion coefficient

$$\frac{E A_i}{L} (C_2 - C_1) = E' (C_2 - C_1)$$



# Example applications

## ❖ Two reactors consist of Lake Huron and Saginaw Bay

- Assuming steady state, estimate the exchange coefficient value  $E'$  using data from Table 1 (handout) for chloride

$$V_2 \frac{dC_2}{dt} = W_2 - Q_2 C_2 + E'(C_1 - C_2)$$

- Formulate the full unsteady model (in Stella) and ensure that it reproduces the steady state concentrations

- ❖ Consider a model for Lake Erie that is based on a division of the lake into its three main basins (see Figure 1 on handout). Develop a model for phosphorus in the three basins using data from Table 1 (handout).
  - You will need to choose settling velocities to try to match the data shown in Table 2 (handout).